High-throughput optofluidic system for the laser microsurgery of oocytes

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Abstract. This study combines microfluidics with optical microablation in a microscopy system that allows for high-throughput manipulation of oocytes, automated media exchange, and long-term oocyte observation. The microfluidic component of the system transports oocytes from an inlet port into multiple flow channels. Within each channel, oocytes are confined against a microfluidic barrier using a steady fluid flow provided by an external computer-controlled syringe pump. This allows for easy media replacement without disturbing the oocyte location. The microfluidic and optical-laser microbeam ablation capabilities of the system were validated using surf clam (Spisula solidissima) oocytes that were immobilized in order to permit ablation of the 5 μm diameter nucleolus within the oocyte nucleolus. Oocytes were the followed and assayed for polar body ejection.

Keywords: microfluidics; optical ablation; high-throughput; long term; microscopy; Spisula solidissima; oocytes; cell division.

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1 Introduction

Performing a long-term and high-throughput developmental analysis of optically manipulated oocytes is difficult. This difficulty may be due to several factors: (1) oocyte nonadherence to microscopy imaging dishes, (2) altered oocyte position over time caused by stage movements and media convection, and (3) the inability to change the culture media without perturbing the location of the oocytes. The most common approach to stabilizing the oocyte is the use of a vacuum (holding) pipette. Since each oocyte requires its own pipette, this method limits the experimental throughput. Oocytes can also be immobilized by adherence to chemically coated coverglasses. This method, however, is prone to cause overadhesion and unwanted cell surface effects. To allow for the high-throughput analysis of experimentally manipulated oocytes over a long time period, an automated optofluidic laser microscopy system has been developed. The fluidic components of the system utilize polydimethylsiloxane (PDMS) soft lithography that was developed a little over 10 years ago. Subsequently soft lithography has been applied to the mechanical characterization of oocytes as well as the production of artificial oocytes. Additionally, over the decade microfluidics have been combined with optics to manipulate various somatic cells. Studies have been performed combining microfluidics with optical ablation for the long-term and high-throughput analysis of oocytes. A system has been created that combines both microfluidics and optical ablation to analyze the structure-function relationship of oocyte organelles. In particular, a validation study was performed where surf clam (Spisula solidissima) oocytes were observed after organelle ablation. These experiments have suggested that a targeted organelle, the nucleolus, controls meiotic cell division in Spisula solidissima oocytes.

First described at least 150 years ago, the nucleolus is a RNA-rich organelle located within the nucleus (Fig. 1). It has a proposed role in the formation of the spindle in cell division. To explore this role, we have used laser microsurgery to damage the nucleolus in Spisula solidissima oocytes. After ablation, cells were exposed to potassium chloride, an artificial parthenogenesis agent, to activate the first steps in meiotic cell division. Potassium chloride works by biochemically activating the M-phase promoting factor system; this causes changes to intracellular calcium dynamics. After laser microablation of the nucleolus the oocytes are maintained in the microfluidic system, and followed to determine whether subsequent ejection of the polar body, an indication of successful meiotic division, had occurred. This experiment validates the use of the optofluidic system for high-throughput optical ablation and subsequent long-term analysis.

2 Materials and Methods

2.1 Optical Design

The laser microablation part of the system consists of a Spectra Physics Duo 210 (337 nm wavelength, 4 ns pulse width, 75 kW peak power, 6 mW average power, 60 Hz repetition rate) nitrogen laser (Newport, Newport, CA, USA) coupled to a Zeiss Observer A1 inverted microscope with a 40× oil immersion (phase III, NA 1.3, EC Plan-Neofluor) objective lens (Carl Zeiss MicroImaging, Thornwood, NY, USA). The objective lens transmission at 337 nm was measured to be ∼40% using a modified dual objective method. The preobjective power was determined...
to be 20 μW using a laser light meter (Thorlabs, Newton, NJ, USA). The laser beam was focused to a diameter of 3 μm in the center of the approximately 5 μm nucleolinus for 1 sec (60 pulses at 60 Hz). The total energy delivered at the focal plane was 8 μJ per pulse energy was 0.13 μJ) with an average irradiance of 1.1×10² W/cm², and a peak irradiance of 4.7×10⁸ W/cm². In addition to phase contrast imaging, the microscope was also equipped with differential interference contrast (DIC) imaging, which allowed for easier visualization of the nucleolinus. Phase and DIC images were captured using an Orca R2 (12-bit, 1344×1024 pixels) CCD camera (Hamamatsu, Hamamatsu, Shizuoka, Japan) mounted on the microscope side port. Image acquisition and laser targeting were controlled using a custom Robolose Labview (National Instruments, Austin, TX, USA) algorithm previously described.18

2.2 Fluidic Design

The oocytes were separated into channels and prevented from moving using microfabricated barriers (see results for a detailed design description). To create the master mold, transparency masks were created in Illustrator (Adobe, San Jose, CA, USA) and printed at 3600 dots per inch (DPI) on transparencies (Stats Prepress, San Diego, CA, USA). The masks were then mounted on 5/16 × 5/16 borosilicate glass (McMaster Carr, Elmhurst, IL, USA) using double-sided tape. In clean-room conditions 10 mL of SU-8 50 (MicroChem, Newton, MA, USA) was poured onto 4/5 silicon wafers (Wafer World, West Palm Beach, FL, USA). The wafers were then spin-coated at 400 revolutions per minute (RPM) at an acceleration of 130 RPM/sec² for 20 sec. Subsequently the speed was increased to 3000 RPM with an acceleration of 260 RPM/sec² for 3 min. This yielded an approximate height of 26 μm, which was enough to trap the surf clam oocytes with diameters of approximately 60 μm. The heights of the channels were measured using a Dektak 150 profilometer (Veeco, Plainview, NY, USA). The wafer was baked at 65°C for 5 min and at 95°C for 15 min to evaporate solvents and stiffen the SU-8. Afterward, 90 sec of UV exposure (0.58 mJ/cm²/sec) through the transparency mask on a mask aligner (Neutronix-Quintel, Morgan Hill, CA, USA) was used to crosslink selected portions of the SU-8 corresponding to the design pattern. The wafer was next baked at 65°C for 5 min and at 95°C for 15 min to enhance SU-8 crosslinking. It was then washed in SU-8 developer (MicroChem) for 6 min to remove the uncrosslinked portions of the SU-8. Wafers were cleaned with isopropyl alcohol and dried with compressed nitrogen. A final bake at 115°C for 1 h was conducted to evaporate any remaining developer and further solidify the SU-8 photoresist.

After baking, a second layer of SU-8 was added and processed using a similar method as the first layer. First, another 10 mL of SU-8 50 was placed on the wafer. The wafer was initially spin-coated at 500 RPM for 20 sec and increased to 1000 RPM for 3 min. This created an additional ~58 μm layer making the total height ~84 μm. This height is sufficient to allow surf clam oocytes to flow through the channels. The wafer was then baked at 65°C for 10 min and at 95°C for 30 min. Subsequently the wafer was exposed to UV light at 0.58 mJ/cm²/sec for 120 sec through the photolithography mask inside the mask aligner. The wafer was next baked at 65°C for 5 min and at 95°C for 25 min. Following this, the wafer was washed with SU-8 developer for 10 min, cleaned with isopropyl alcohol, and dried with compressed nitrogen. It was then baked at 115°C for 1 h.

Sylgard 184 silicone elastomer base was mixed with Sylgard 184 curing agent in a 10:1 w/w ratio (Dow Corning, Midland, MI, USA). Bubbles were removed from the mixture using a vacuum desiccator. In a separate desiccator, 2 mL trichloro-methylsilane (Sigma-Aldrich, Saint Louis, MO, USA) was evaporated onto the master mold to allow for an easier release of the elastomer. The resulting elastomer mixture was poured onto the master mold and cured at 80°C for 20 min. After curing, the elastomer was peeled off and trimmed. A 3 mm skin biopsy punch (Acuderm, Fort Lauderdale, FL, USA) was used to create the input hole and a 20 gauge (0.603 mm inner diameter and 0.908 mm outer diameter) blunt-tip needle (McMaster Carr) was used to create the output hole. The microfluidic chamber was mounted onto a 50×45×0.15±0.02 mm cover glass (Thermo Fisher Scientific, Waltham, MA, USA). The outlet port was connected to a dual-syringe infusion/withdrawal pump (KD Scientific, Holliston, MA, USA) via 0.79 mm inner diameter and 2.4 mm outer diameter Tygon tubing (Saint-Gobain, Courbevoie, France). The syringe pump was used in the withdrawal mode to pull the input solution through the channel. Syringe pump actuation was controlled by a custom Labview algorithm using RS-232 commands (9600 baud rate, 8 data bits, no parity, no flow control) called by Labview’s VISA (Virtual Instrument Software Architecture) functions.

2.3 Fluidic Validation Using Beads

Prototype microfluidic chambers were fabricated as described in Sec. 2.2. Polystyrene beads (Duke Scientific, Palo Alto, CA, USA) with diameters of 59.1 μm ± 0.9 μm were used to mimic oocytes during barrier testing. During the testing of the media changing, solutions of phosphate buffer solution (PBS) and 1 mM fluorescein in PBS (Sigma-Aldrich, Saint Louis, MO, USA) were interchanged. Fluorescence imaging was conducted using the Observer A1 microscope and Orca R2 camera described in Sec. 2.1. Fluorescent excitation was provided by an X-Cite 120 mercury vapor short arc lamp.
and was coupled through a EGFP filter cube (Chroma Technology, Bellows Falls, VT, USA).

2.4 Optofluidic Validation Using Oocytes

Gravid surf clams, Spisula solidissima, were provided by the Marine Resources Center at the Marine Biological Laboratory (Woods Hole, MA, USA). Ovaries were dissected to release oocytes, which were rinsed in 0.45 μm filtered seawater. Immediately after washing, oocytes were shipped on ice overnight for experimentation and analysis in San Diego. At room temperature, oocytes were loaded into the microfluidic chamber and ablated as described in Sec. 3.3. After irradiation, the oocytes were exposed to 0.07 M KCL by adding 0.5 M KCL into the media. Cells were observed for 50 min to determine whether or not polar body ejection had occurred. In addition to irradiation/ablation of the nucleolus, two series of controls were performed: (1) no irradiation, and (2) irradiation inside the nucleolus but outside of the nucleolus. A chi-square test was used to compare the nucleolus-irradiated cells with the control cells.19

3 Results

3.1 Microfluidic Design

The microfluidic chamber allows for the high-throughput long-term analysis of oocytes following laser microirradiation of the nucleolus (Fig. 2 and Fig. 3). Oocytes are initially loaded into the inlet port of the microfluidic chamber. Employing Labview, the syringe pump is operated to draw the oocytes into the channels and against the barrier (Fig. 4). By leaving the syringe pump on, a continuous flow of fresh media and oxygen can reach the cells. This constant flow is beneficial for oocytes, which require oxygen for successful development.20,21 Also the media can be easily exchanged by switching the media in the inlet port.

A key design consideration was the choice of device materials. For precise optical ablation it is essential to use a high numerical aperture (NA) objective for focusing the laser into the oocyte. The laser ablation portion of the system uses an inverted microscope with a 1.3 NA oil immersion objective which requires pairing with a 0.15 ± 0.02 mm thick cover glass. These thin cover glasses are used due to the short working distances of high NA objectives. This ablation requirement forces the microfluidic device to use this cover glass for its base. Other materials would not be able to match the index of refraction or the uniform thickness provided by the glass. The rest of the chamber was comprised of PDMS due to its ease of manufacture, high optical transparency, and low toxicity.5,6,22 Oocyte viability was investigated in this new device environment with unnatural surface wetting and mechanical properties. Compared to control oocytes in standard glass-bottom dishes, oocytes in the microfluidic chambers showed similar cell morphology and polar body ejection rates. The health of the oocytes within the microfluidic chamber is likely due to both the low toxicity of the PDMS and the oocyte’s nonadherent membrane minimally interacting with the device surfaces.

An additional microfluidic design consideration was the choice between a single layer-based vertical barrier and a...
multilayer-based horizontal barrier. A single-layer approach with a channel width beginning at >60 μm and decreasing to 26 μm also would have allowed for the confinement of the oocytes. This method, however, provides a less favorable flow field for use with optical ablation. In the single-layer approach, the flow field that pushes the oocyte against the barrier is equal along the height of the channel. There may be situations where an oocyte can be confined against the barrier distant from the cover glass and outside of the working distance of the objective. To force all the oocytes to be at a uniform depth in a single-layer design, the channel height would need to be approximately the diameter of the 60 μm oocyte. Using this channel height, viscous drag against the channel would severely limit the flow rates of the oocytes within the channel. A multilayer approach was instead used in which the flow field is directed toward the cover glass as it flows under the barrier. This flow pattern keeps the oocytes close to the bottom cover glass.

3.2 Fluidic Validation Using Beads

A proof-of-principle experiment was performed using a prototype microfluidic chamber. In this experiment, 59.1 μm ± 0.9 μm polystyrene beads that represent oocytes in shape and dimension were loaded into the microfluidic chamber [Fig. 5(a)]. Upon reaching the barrier, it was determined that the beads remained in a fixed position. [Fig. 5(b)–5(c)]. Additionally, a fluorescein solution was washed in and out of the chamber in order to validate the media-changing capabilities [Fig. 5(d)–5(g)].

3.3 Optofluidic Validation Using Oocytes

In the nonlaser control experiments, polar body ejection occurred in 135 of the 154 (87.7%) of the oocytes (Table 1). In the controls where the nucleolus was irradiated, there was a polar body ejection in 80 out of the 96 (83.3%) oocytes. In the nucleolinus-irradiated oocytes, polar body ejection occurred in 68 out of the 100 (68%) oocytes. Using a chi-squared test, the nucleolinus ablated population was determined to be statistically different from the control populations (P < 0.05). Of a total of

<table>
<thead>
<tr>
<th>Location</th>
<th>Polar body ejection</th>
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<tbody>
<tr>
<td>Location</td>
<td>Yes</td>
</tr>
<tr>
<td>No cut (Control)</td>
<td>135</td>
</tr>
<tr>
<td>Nucleolus (Control)</td>
<td>80</td>
</tr>
<tr>
<td>Nucleolinus</td>
<td>68</td>
</tr>
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302 oocytes exposed to the laser, 106 (35.1%) lysed upon laser exposure and were removed from the data sets. Lysis was likely due to the high threshold laser powers required to damage the nucleolinus. This lysing was the reason that the laser power was not increased further to obtain more significant results in Table 1.

4 Discussion
Optical ablation is an effective noninvasive method used to perturb intracellular organelles. This method, however, has limited use when working on oocytes due to the oocyte’s nonadherent nature. To overcome this limitation, a custom microfluidic chamber and automated fluid handling was incorporated into the laser microscopy system. A preliminary validation experiment was performed to test the capabilities of the microfluidic system. It was determined that, using microfluidics, it was possible to confine nonadherent oocytes in a single location while constantly exchanging media through the chamber.

A subsequent study was performed utilizing both optical ablation and microfluidics on live oocytes. This study validated the system and supports the results of a recent study showing that the nucleolinus plays an important regulatory role in polar body ejection and the completion of meiosis in the surf clam. In our study, nucleolinus-ablated oocytes had inhibition of polar body ejection with statistical significance ($P < 0.05$) over the two control groups. The fact that 68% of the nucleolinus-irradiated oocytes still ejected their polar bodies is likely due to the fact that, in many cases, the nucleolinus was only partially damaged, thus allowing it to maintain adequate function during polar body ejection. This partial damage could have been caused by variations in the delivered laser dose or by the fact that the 3 μm diameter focused laser spot was not sufficiently large enough to damage the larger 5 μm diameter nucleolinus. Additionally, differences in nucleolinus position and depth within the 60 μm diameter oocytes might have caused laser-light scattering differences significant enough to affect the irradiance reaching the target. Additionally, overnight shipment across the country may have disrupted normal oocyte function. Despite these potential problems, the results strongly suggest ($P < 0.05$) a correlation between damaging/destroying the nucleolinus and impaired oocyte polar body ejection. This has been confirmed and reported in subsequent studies using a different laser system and not requiring shipment of oocytes across the United States.

In summary, an optofluidic system has been developed that allows for the high-throughput long-term analysis of oocytes. This system can now be used to study other early embryonic processes by combining microfluidics with optical manipulation methods such as laser microablation (scissors) and laser trapping. Such a system may find widespread use in livestock husbandry, and eventually in human in vitro fertilization (IVF). Additionally, the system can be further expanded for use in cell microsurgery, combined trapping and microsurgery, and for studies on nonadherent cell types.

Acknowledgments
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References